



RESEARCH ARTICLE

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Key Points:

- This study forecasts probabilistic short-term system scale irrigation demand for lead time up to 5 days
- Measurement/estimation/forecast errors for flows, NWP forecasts and observed weather are integrated
- Rank histograms and other indices indicated that a reliable ensemble spread is achieved.

Supporting Information:

- Supporting Information S1

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Ensemble forecasting of short-term system scale irrigation demands using real-time flow data and numerical weather predictions

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Abstract Irrigation demands fluctuate in response to weather variations and a range of irrigation management decisions, which creates challenges for water supply system operators. This paper develops a method for real-time ensemble forecasting of irrigation demand and applies it to irrigation command areas of various sizes for lead times of 1 to 5 days. The ensemble forecasts are based on a deterministic time series model coupled with ensemble representations of the various inputs to that model. Forecast inputs include past flow, precipitation, and potential evapotranspiration. These inputs are variously derived from flow observations from a modernized irrigation delivery system; short-term weather forecasts derived from numerical weather prediction models and observed weather data available from automatic weather stations. The predictive performance for the ensemble spread of irrigation demand was quantified using rank histograms, the mean continuous rank probability score (CRPS), the mean CRPS reliability and the temporal mean of the ensemble root mean squared error (MRMSE). The mean forecast was evaluated using root mean squared error (RMSE), Nash–Sutcliffe model efficiency (NSE) and bias. The NSE values for evaluation periods ranged between 0.96 (1 day lead time, whole study area) and 0.42 (5 days lead time, smallest command area). Rank histograms and comparison of MRMSE, mean CRPS, mean CRPS reliability and RMSE indicated that the ensemble spread is generally a reliable representation of the forecast uncertainty for short lead times but underestimates the uncertainty for long lead times.

1. Introduction

Short-term system scale irrigation demand forecasts are extremely useful for system operators to make irrigation water distribution decisions, but they are subject to uncertainties resulting from input parameters and model structure. Parameter and structural uncertainties are inherent in models, as models try to simplify the complex reality. Input uncertainties are also important as inputs are subject to measurement, estimation or prediction uncertainties. From the irrigation demand forecasting perspective, uncertainties in the irrigation demand forecasts can result from observation, estimation or prediction uncertainties in biophysical (crop-soil-climate interaction), behavioral (farmers and system operators attitude that influencing management decisions) and supply (supply source, seasonal allocation, permanent entitlement) factors [Zaman *et al.*, 2007]; as well as from the respective parameter uncertainties, depending on the specific models used. This research makes ensemble forecasts of irrigation demand using a multivariate time-series model of short-term (up to 5 days) daily irrigation demand forced by observed demands and observed and forecast weather integrating measurement errors, estimation errors, and weather forecast uncertainty.

Past research has used sophisticated and highly complex modelling architectures such as process-based (conceptual) and data-driven (statistical) approaches [Alfonso *et al.*, 2011; Pulido-Calvo and Gutierrez-Estrada, 2009] to derive irrigation demand forecasts. Typically, process-based approaches have been used at field scale and data-driven approaches have been used at system scale. Few of these studies have attempted to estimate irrigation demand forecast uncertainties. Studies at the system scale have mainly used data-based deterministic models to forecast irrigation demand [Pulido-Calvo and Gutierrez-Estrada, 2009; Pulido-Calvo *et al.*, 2007; Pulido-Calvo *et al.*, 2003]. A few of these studies have considered uncertainty, mainly focusing

on parameter uncertainties. Both bootstrap methods [Ticlavilca *et al.*, 2011] and Bayesian techniques [Alfonso *et al.*, 2011] have been used to investigate the irrigation demand forecast uncertainties resulting from model parameters. Also, some univariate time series models based on previous irrigation flows [Pulido-Calvo and Gutierrez-Estrada, 2009; Pulido-Calvo *et al.*, 2003, 2007] have captured the combined uncertainty from inputs and model structure by including the associated error model to represent the random error component in the irrigation demand forecasts.

Many models have used short-term weather forecasts to make irrigation decisions, especially precipitation [Azhar and Perera, 2011; Cai *et al.*, 2011; Gowing and Ejieji, 2001; Wang and Cai, 2009; Wilks and Wolfe, 1998], temperature [Ticlavilca *et al.*, 2011; Wilks and Wolfe, 1998] and evapotranspiration [Alfonso *et al.*, 2011; Tian and Martinez, 2014]. Weather forecasts have often been considered for field scale and a few studies that we are aware of have incorporated weather forecasts at the system scale [Tian and Martinez, 2014]. Field scale models have often used weather forecasts for irrigation scheduling (i.e., predict timing and its volume) and weather forecast uncertainties were manifest mainly in variations of the irrigation timing [Cai *et al.*, 2011; Gowing and Ejieji, 2001; Wang and Cai, 2009; Wilks and Wolfe, 1998]. These models only used limited forecast information as the quality of the available weather forecast at that time was poor at longer lead times (greater than 3 days lead times) [Gowing and Ejieji, 2001]. This was seen as a major impediment at the time. Alfonso *et al.* [2011] and Tian and Martinez [2014] forecasted system scale irrigation demands, combining stochastic reference evapotranspiration forecasts derived from a machine learning algorithm and currently operational Global Ensemble Forecast System (GEFS), respectively. Ticlavilca *et al.* [2011] also combined daily maximum and minimum temperature with system scale irrigation demand forecasts using a machine learning algorithm.

These system scale models were mainly developed for arid-zone agriculture and precipitation forecasts were not considered, as it is not important for irrigation decisions in those environments [Alfonso *et al.*, 2011; Tian and Martinez, 2014; Ticlavilca *et al.*, 2011]. These studies have generated system scale stochastic irrigation demand forecasts with prediction intervals. In terms of assessing the probabilistic forecasts, all studies provided a graphical comparison of observed time series overlain on the forecast prediction intervals without a quantitative evaluation. Tian and Martinez [2014] also provided relative operating characteristic (ROC) diagrams that suggested, they didn't provide any statistical analysis of the reliability or sharpness of the probabilistic forecasts. The maximum lead time for the most of these studies was 2 days or less and no study comprehensively integrates input uncertainties into the irrigation demand forecast uncertainties. While ensemble techniques have been used elsewhere, in hydrology [e.g. Addor *et al.*, 2011; Li *et al.*, 2015; Shrestha *et al.*, 2013a; Zappa *et al.*, 2011] and hydrometeorology [e.g. Brown *et al.*, 2010; Ebert *et al.*, 2011; Gneiting, 2013; Robertson *et al.*, 2013a; Rossa *et al.*, 2011], no studies we are aware of have used both stochastic precipitation and reference evapotranspiration forecasts nor have there been studies that combine uncertainties in antecedent flows and observed and forecast weather to derive stochastic volumetric irrigation demand forecasts at system scale.

Ensemble techniques are commonly used to represent uncertainty in nonlinear models. In the context of forecasting; ensemble forecasting is a form of Monte Carlo analysis that is used to characterize uncertainty in model outputs [Toth and Kalnay, 1993]. In principle, this technique can be applied for both input and parameter uncertainty depending on the context of the modelling. Ensemble forecasting techniques have been widely used in science, engineering, medicine and ecology, among other areas. It has been widely used in weather forecasting [Ebert, 2001; Ebert *et al.*, 2011; Gneiting, 2013; Gneiting and Raftery, 2005] and species distribution modelling [Araújo and New, 2007; Buisson *et al.*, 2010; Grenouillet *et al.*, 2011; Thuiller *et al.*, 2009] to capture errors in the initial condition and model structure. In the field of water resources engineering, ensemble forecasting techniques have also been used extensively in forecasting stream flow [Bennett *et al.*, 2014], short-term water demand [Hutton and Kapelan, 2015] and floods [Alvarez-Garretón *et al.*, 2014; Cloke and Pappenberger, 2009; Li *et al.*, 2014; Schaake, 2006; Schaake *et al.*, 2005]. In these studies, sources of uncertainty included in forecast ensembles were uncertainty in inputs (mainly precipitation forecasts), state variable (soil moisture), and model structures through model parameters. We are unaware of any irrigation demand forecast model that has used ensemble forecasting techniques to derive stochastic irrigation demand forecasts.

The structure of the multivariate time series model used here, which has auto-correlated and cross-correlated multivariate inputs, some of which are nonlinearly transformed, suggests ensemble forecasting

techniques to derive output uncertainties would be useful. This technique has advantages in multivariate time series models compared with the bootstrap method, which can often distort the cross correlations between multivariate inputs and outputs [Khaliq *et al.*, 2009; Rummel *et al.*, 2010], whereas ensemble forecasts can preserve the error covariance among input time series which is then transferred through the regression structure to the stochastic output. However, the outcomes from an ensemble forecasting technique is dependent on the quality of the input time series. Therefore, a good quality data set (i.e., fine scale, free from bias and complete) is important for generating reliable, unbiased output ensembles. Past impediments such as the lack of required data, the expense of data acquisition and low data quality are being reduced with the availability of irrigation flow data from fully automated irrigation distribution systems, short-term weather forecasts from numerical weather predictions (NWP) models and observed weather data from automatic weather stations. In particular, the accuracy of the weather forecasts is continuously improving and consistent real-time irrigation flow data are now available from modernized distribution systems. This provides an opportunity to apply ensemble forecasting techniques to generate stochastic irrigation demand forecasts.

This paper develops ensemble irrigation demand forecasts using the irrigation distribution system in the Goulburn-Murray Irrigation District (GMID) in Northern Victoria as a case study. This system has been modernized and automated connections provide consistent real-time flow data [NVIRP, 2010a]. Previously, Perera *et al.* [2015a] developed a deterministic model and assessed its performances under perfect weather forecasts i.e., using observed weather data. This paper uses that model as a basis and both brings real weather forecasts into the analysis and develops an ensemble framework to incorporate uncertainties arising from the weather forecast data as well as other inputs. In doing this we use data from the GMID and numerical weather predictions (NWP) from the Bureau of Meteorology (BOM) to develop ensemble irrigation demand forecasts. This is a relatively new and high level of data availability compared with many irrigation systems. The analysis includes input uncertainties associated with the flow measurement and weather measurements and forecasts. The remainder of the paper describes the area of study where the methodology has been applied and forecasting performance for command area driven stochastic irrigation demand forecasts and conclusions that has been drawn. This provides novel understanding about the irrigation demand prediction uncertainties like input uncertainties related to biophysical, behavioral and supply factors and in turn assists system operators to mitigate the risk associated with their routine irrigation distribution decisions.

2. Study Area and Data

2.1. Study Area

The study area and data sources are described in detail in Perera *et al.* [2015a]. The study area is located in the Central Goulburn Irrigation District (CGID), Victoria, Australia. Agriculture in the study area is dominated by irrigated dairy, pome and stone fruit production, with other agricultural activities related to sheep for wool, beef and dairy cattle [RDV, undated]. The main source of water supply for the CGID is from Lake Eildon, with delivery via the Goulburn River, Goulburn weir, and the Stuart Murray Canal. Water flows from Stuart Murray Canal to the CGID through six gravity irrigation distribution channels namely CG1, 2, 3, 4, 5 and 6. Any excess water in the Stuart Murray Canal is diverted to Waranga Basin (Figure 1). The irrigation distribution system in the CGID is highly automated and a SCADA (supervisory control and data acquisition) system monitors levels and flows and controls the regulator gates and meter outlets across the district. Irrigation water takes about 4 days to travel from Lake Eildon to the farms in this area. The proposed ensemble forecasting methodology was applied to 287 km² of irrigated agricultural land supplied by CG 1, 2, 3 and 4. The characteristics for each channel are given in Table 1. The irrigation year starts on the 15 of August and continues to the 15 of May the following year. The study area is approximately 110 meters above the Australian height datum (AHD) and the climate is temperate with a hot summer ($T_{hot} \geq 22^{\circ}\text{C}$) but without a dry season (Köppen climate type Cfa) [Peel *et al.*, 2007].

2.2. Data Sources and Preprocessing

2.2.1. Irrigation Flow Data

The irrigation flow data related to the regulators and service points were collected from the operational SCADA system known as Total Channel ControlTM (TCCTM) that is used by Goulburn-Murray Water

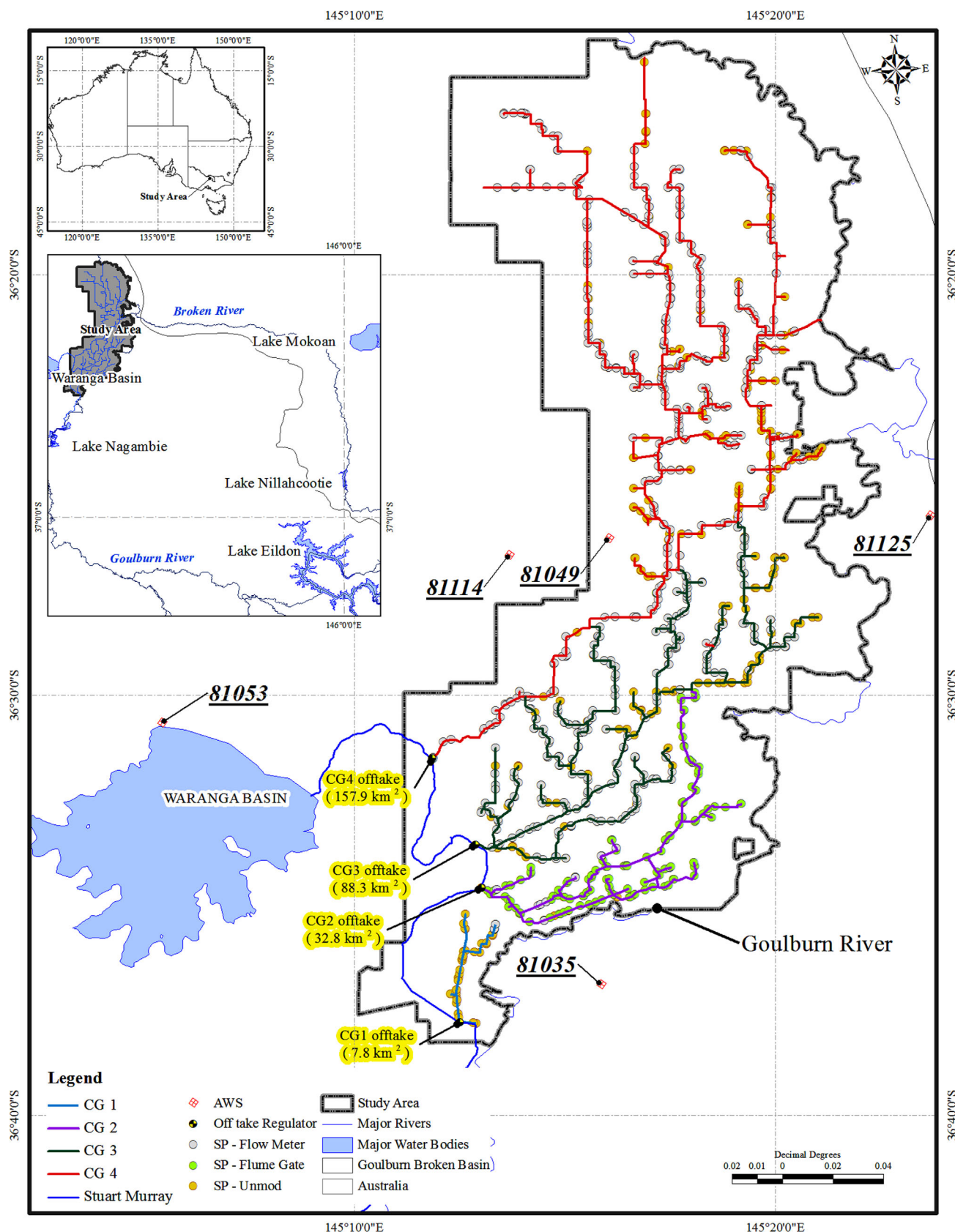


Figure 1. Study area—Central Goulburn channel 1, 2, 3, and 4 [Perera et al., 2015a].

Table 1. Characteristics of CG 1, 2, 3 and 4 Channels

Channel	Length(km)				Area (km ²)	Service Points (Nos.)			Regulators (Nos.)			Degree of Mod. ^b (%)	
	L ^a –1	L ^a –2	L ^a –3	Total		Mod. ^b	Unm. ^c	Total	Mod. ^b	Unm. ^c	Total	SP ^d	Vol ^e
CG1	5.5	2.4		7.87	7.8	5	41	46	5	3	8	11	20
CG2	18.5	15.6	3.2	37.3	32.8	142	7	149	36	0	36	95	96
CG3	17.32	43.34	25.5	86.2	88.3	246	109	355	88	17	105	70	65
CG4	39.8	76.9	23.4	140.0	157.9	357	109	466	117	32	149	77	60
CG1234	81.1	138.2	52.1	271.4	286.9	750	266	1016	246	32	298	74	65

^aLevels of distribution (L-1- backbone, L-2–primary and L-2–secondary).

^bModernized.

^cUnmodernized.

^dService points.

^eVolume through automated service points.

(GMW). TCCTM is a fully automated open channel delivery system that captures flow measurements in real-time at all regulating structures and farm supply points. We used the flow data recorded at 1016 supply points for the period 15 August 2006 to 15 May 2012; which includes 6 irrigation years. The service point delivery data were aggregated to a daily time step. The SCADA system records the start and end times and flow rates of irrigation order deliveries. Service point flows were aggregated across all service points for each individual channel and the study area as a whole. This aggregation implicitly assumes that the travel time along the local channel or study area is significantly less than a day. The aggregated service point flows are denoted $ID_{CGi, ASP}$. Here “ASP” denotes the Aggregated Service Points, and “i” provides spatial aggregation area (where $i=1, 2, 3, 4$ or 1234).

2.2.2. Observed Climate Data

The observed climate data were obtained from two Automatic Weather Stations (AWSs) and three daily read rain gauge sites operated by the Australian Bureau of Meteorology (BoM) [BoM, 2005] located in and around the study area (Figure 1). The characteristics of each weather station are given in Table 2. Daily precipitation records were collected from all five sites as the area often witnesses localized patchy precipitation events. These five sites were established well before the channel automation and record start dates vary between 1883 and 1996. The hourly weather variables needed to estimate daily reference evapotranspiration– ET_0 were collected from the AWSs (air temperature, dewpoint temperature, wind speed) and satellite imagery (solar radiation) as described by Perera *et al.* [2014, 2015b]. The measurement ranges and accuracies of these observed weather variables are given in Table 3. The AWSs and rain gauges nominally provide continuous measured weather data; however, there were times within the study period when hourly/daily weather data were missing due to various reasons. For missing daily precipitation, the aggregated value recorded at the end of missing period was uniformly disaggregated over the missing period, while other weather variables were infilled from the neighbouring AWS.

Table 2. Characteristics of Automatic Weather Stations and Rain Gauges

No.	AWS no.	Name	Latitude (degrees)	Longitude (degrees)	El. (m)	Precip. ^a	T ^b , Dew ^c , WS ^d and SRad ^e
1	81125	Shepparton Apt. ^f	–36°25′44″	145°23′41″	113.9	✓	✓
2	81049	Tatura Inst. ^g sus. ^h ag ⁱ	–36°26′16″	145°16′02″	114.0	✓	✓
3	81114	Thiess Service	–36°26′40″	145°13′40″	114.0	✓	×
4	81053	Waranga Reservoir	–36°30′39″	145°05′25″	121.0	✓	×
5	81035	Murchison	–36°36′53″	145°12′51″	115.0	✓	×

^aPrecipitation.

^bDaily temperature.

^cDew point temperature.

^dWind speed.

^eSolar Radiation.

^fAirport.

^gInstitute.

^hSustainable.

ⁱAgency.

Table 3. Measurement Range and Accuracy of Climate Variables From AWS [BoM, 2005]

Sensor	Range	Accuracy	Unit
Air pressure	750 to 1060	0.3	hPa
Air temperature	−25 to +60	0.3	°C
Wet bulb temperature	−25 to +60	0.3	°C
Relative Humidity	2 to 100	3	%
Wind Speed	2 to 180	2	knot
Wind Direction	0 to 359	5	degree
Precipitation	0 to 999.8	2%	mm

2.2.3. Weather Forecasts

The short-term weather forecasts relevant for the study area were collected from the Australian Bureau of Meteorology's operational NWP forecasts derived from the Australian Community Climate and Earth System Simulator–(ACCESS) [Puri *et al.*, 2013]. The ACCESS systems are nonhydrostatic, hybrid vertical level structure, mesoscale assimilation & forecast systems. They have been operational since 17 August 2010. The temporal (lead time) and spatial resolution for different ACCESS systems vary from +1 to +240 h and 5 to 80 km, respectively. The forecast performances for precipitation and mean sea level pressure of the ACCESS systems have been comprehensively evaluated [BoM, 2010, 2012; Puri *et al.*, 2013] and also its outputs have been extensively used for short-term stream flow forecasting [Pagano *et al.*, 2010; Shrestha *et al.*, 2012, 2013b]. We selected the ACCESS-G system, which has the largest lead time (+240 h) and the largest grid cells (80 km) in order to derive irrigation demand forecasts for longer lead times, where the next higher resolution model has a lead time of only 72 h. ACCESS-G is run twice a day providing forecasts starting at 10:00 AM and 10:00 PM local time (i.e., 0000 and 1200 UTC). The outputs from these runs are available at 03:50 PM and 03:50 AM (the next day), respectively [BoM, 2010]. We used the 10:00 AM local time run and constructed 9 midnight to midnight daily ET_O and 09:00 AM to 09:00 AM daily precipitation forecasts using the 3 hourly NWP forecast outputs of precipitation, air temperature, dew point temperature, wind speed and incoming solar radiation from 17 August 2010 to 1 August 2012. The four grid points surrounding the station were linearly interpolated to the AWS location and biases in the forecast ET_O input variables were corrected following Perera *et al.* [2014] and precipitation forecasts were post-processed following Robertson *et al.* [2013b]. The ET_O forecasts have been evaluated in detail by Perera *et al.* [2014], who found that the root mean squared error (RMSE) and coefficient of determination (R^2) values ranged over 0.73–1.43 mm d^{−1} and 0.91–0.01 for 1 and 9 day lead times, respectively. Precipitation forecasts have R^2 values of 0.65 and 0.55 for 1 and 3 day lead times, respectively [BoM, 2010].

3. Methodology

In this paper, the multivariate time series model developed previously by Perera *et al.* [2015a] is used to derive irrigation demand forecast ensembles for lead time up to 5 days. In principle, the ensemble forecasting approach can include all sources of uncertainties. We undertook some preliminary evaluations to decide which uncertainties to incorporate in this analysis (not presented). This involved perturbing model inputs and parameters individually and collectively and examining the output ensemble spread. It was found that including both model input and parameter uncertainty did not significantly change the ensembles compared with only including model input uncertainty. Including only parameter uncertainty led to very narrow output ensembles. Therefore, the ensemble forecast approach used here was simplified by omitting the parameter component.

Figure 2 provides the schematic diagram of the ensemble forecast approach that has been adopted and shows the flow of input data through to ensemble irrigation demand forecasts along the time line. Steps 1–3 are about characterizing the statistical structure of each input time series, including measurement error characterization; correction of NWP forecast bias and characterization of NWP forecast uncertainty, followed by creation of the input ensembles for each model input. We used different perturbation methods in order to account for measurement, observation and forecast uncertainties given that the deterministic multivariate time series model is forced by observed demands and observed and forecasted weather. The selected perturbation methods are discussed in detail later in this section. We post-processed input ensembles using the Schaake Shuffle method [Clark *et al.*, 2004] to achieve realistic cross-correlations and temporal

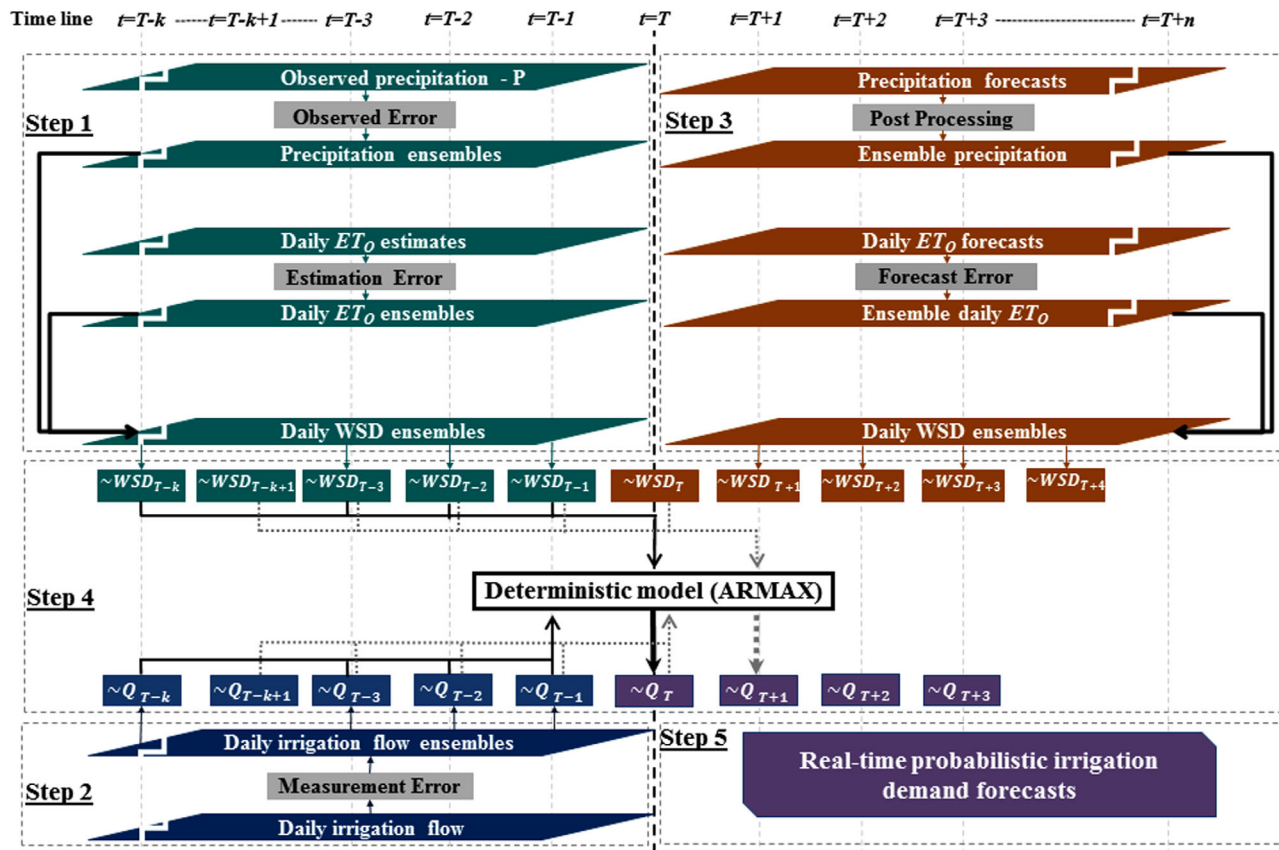


Figure 2. The schematic diagram of the ensemble forecast approach.

persistence within each ensemble. Step 4 involves preparing past and future forcing variable (water supply deficit) and running the deterministic ARMAX models with the various input ensembles. A brief description of the deterministic model and its calibration is given in the next section and further details can be found in Perera *et al.* [2015a]. Step 5 summarizes the daily ensemble irrigation demand forecasts into a probabilistic irrigation demand forecasts.

The various modelling steps above are described in more detail in the following methodology sections. The last part of the methodology describes the evaluation methods that have been used to quantify the forecast performance of ensemble irrigation demand forecast.

3.1. Deterministic Model and its Calibration

3.1.1. Deterministic Model Structure

The model used here is a multivariate time series model, which has been previously developed to derived irrigation demand forecasts for the same study area [Perera *et al.*, 2015a]. This time series model combines bio-physical factors (weather) as the exogenous variable with behavior factors captured through the autoregressive process dependent on immediate past irrigation demands. The model is an autoregressive moving average model with an exogenous variable-(ARMAX) (equation (1)).

$$ID(t) + a_1.ID(t-1) + \dots + a_{n_a}.ID(t-n_a) = b_1.u(t-n_k) + \dots + b_{n_b}.u(t-n_k-n_b+1) + c_1.e(t-1) + \dots + c_{n_c}.e(t-n_c) + e(t) \quad (1)$$

where, $ID(t)$ is the daily irrigation demand at time t , $u(t)$ is the daily exogenous variable at time t , n_a is the number of past irrigation demand terms included, n_b is the number of time points at which the exogenous term is specified plus 1, n_c is the number of autoregressive error terms, n_k is the number of input samples that occur before the input affects the output, also called the dead time in the system, $ID(t) \dots ID(t-n_a)$ are the previous outputs on which the current output depends, $u(t-n_k) \dots u(t-n_k-n_b+1)$ are the

previous and delayed inputs on which the current output depends, $e(t) \dots e(t-n_c)$ are the white-noise disturbance values, which is modeled as an independent and identically distributed (iid) Gaussian process, with zero mean and variance σ_e^2 .

The exogenous variable (u) is a water supply deficit (WSD) index which reflects the effect of atmospheric forcing on irrigation demand as a combination of precipitation and ET_O . The WSD is estimated using a simple soil water bucket model with two parameters.

$$WSD_t = ET_{Ot} \times \left[1 - \left(\frac{S_t}{S_{\max}} \right)^\gamma \right] \quad (2)$$

The storage at time t , S_t , is calculated using a soil water balance,

$$S_t = \min \left(S_{t-1} + P_{t-1:t} - ET_{Ot-1:t} \left(\frac{S_t}{S_{\max}} \right)^\gamma, S_{\max} \right) \quad (3)$$

where, ET_O (mm d^{-1}) is the daily reference crop evapotranspiration, S_t (mm) is the soil moisture storage, S_{\max} is the maximum soil moisture storage (mm), P (mm) is the precipitation. The bucket capacity (S_{\max}) and the nonlinearity (γ) of actual evapotranspiration are determined in the model fitting. WSD is essentially a command area average index aiming to represent the pattern of supplemental water that would need to be supplied through irrigation.

3.1.2. Deterministic Model Calibration

A detailed description of the model fitting and selection through cross validation is provided in *Perera et al.* [2015a]. This included developing data transformation to remove seasonality and scaling differences in the raw data set. Then, the model parameters were estimated in two steps: the first of which determined the order of each transfer function and S_{\max} and γ ; and the second of which determined the lag coefficients. Model selection was guided using the Bayesian information criterion (BIC)

$$\text{BIC} = N \cdot \log \text{MSE} + d \cdot \log N \quad (4)$$

where, MSE is the mean squared prediction error, d is the number of parameters and N is the number of observations.

This is essentially a mean squared error minimization penalized by parameter number as a measure of model complexity. The deterministic model calibration process used a leave-one-year-out cross-validation (LOOCV) technique to select the best time series models based on the BIC calibration. In the original paper [Perera et al., 2015a] 6 years of data were used (calibration on 5 years, validation on 1 year); however, the NWP weather forecasts from ACCESS-G are only available the 2010–2011 and 2011–2012 irrigation seasons due to changes in the Bureau's NWP systems. Therefore this study focusses on just two of the original models; the ones that were validated on the 2010–2011 and 2011–2012 irrigation seasons. Cross-validations showed that the overall patterns between command areas and years were similar. The average performances for RMSE and NSE during calibration, among six cross-validation scenarios across 5 command areas ranged from 2.33 ML d^{-1} (CG 1) to 28.5 ML d^{-1} (CG 1234) and from 0.55 (CG 1) to 0.93 (CG 1234) respectively, for 1 day lead time [Perera et al., 2015a].

3.2. Ensemble Generation

3.2.1. Real-Time Flow Data

The measurement uncertainty for the irrigation flows was estimated from the manufacture's specifications and in-field audits. The measurement uncertainty for automated off take regulators and meter outlets is $\pm 2.5\%$ (95% confidence) under laboratory test conditions [Rubicon Water, 2014]. However, under operational conditions, the Total Channel ControlTM (TCCTM) SCADA system was assessed as being able to maintain a constant rate of flow as channel level varied. Specifically, the field assessment concluded that "the modernised backbone will deliver a uniform flow within $\pm 5\%$ more than 90% of the time" [NVIRP, 2010b]. We have interpreted these two sources of information as representing likely bounds on the in-field performance of the system and we consider error scenarios between these bounds. The above statements imply measurement error standard deviations (as a proportion of measured flow) of 0.0304 ($\pm 5.0\%$ with 90% confidence) and 0.0128 ($\pm 2.5\%$ with 95% confidence) respectively, assuming a normal distribution. A preliminary evaluation (not presented) was carried out to select the measurement uncertainty standard deviation for generating ensembles

of observed flow. This evaluation considered standard deviations of 0.0304, 0.025, 0.02, 0.015 and 0.0128. The results shows the standard deviation for measurement error for and meter outlets of 0.02 (i.e., 2% of measured flow) generated reasonably reliable 1 day lead time forecast ensembles under calibration conditions. This measurement uncertainty is assumed to be a constant proportional error across the full range of flows.

In addition, the measurement errors under laboratory conditions [Rubicon_Water, 2014] and supply error in the field [NVIRP, 2010b] need to be generalized across all the automated off take regulators and meter outlets as regulators record times of flow rate change and meter outlets record the start and end timings and flow rates of irrigation order deliveries. The off take regulator and aggregated service point flow ensembles were created similarly, perturbing daily irrigation flow time series with an additive percentage error. The additive error is assumed to be a white noise. The variance is adjusted for the daily aggregated service point ($ID_{CGi, ASP}$) data, given that it is the sum of many individual service points with individual errors that were assumed to be independent of each other. Therefore, the irrigation flow ensembles for daily aggregated service point ($ID_{CGi, ASP}$) are derived using equations (5) and (6).

$$ID_{CGi, ASP}^{ens} = ID_{CGi, ASP} + \zeta_{CGi, ASP}^{ID} \quad (5)$$

$$\zeta_{CGi, ASP}^{ID} \sim \mathcal{N} \left(0, \sigma_{CGi, ASP}^2 \right) \text{ and } \sigma_{CGi, ASP} = 0.02 \sqrt{\sum ID_{CGi, ASP}^2} \quad (6)$$

where, $ID_{CGi, ASP}^{ens}$ is the irrigation demand ensemble for aggregated service, $ID_{CGi, ASP}$ is the daily aggregated service point, and $\zeta_{CGi, ASP}^{ID}$ is the Gaussian additive noise representing measurement error with zero mean and a variance of $\sigma_{CGi, ASP}^2$. The variance derives from assuming that the 99% measurement confidence interval is $\pm 5.0\%$ of the measured flow.

3.2.2. Observed Weather Variables

The errors in the atmospheric forcing variables for the WSD are a key component contributing to uncertainties in the irrigation demand estimation and forecasting. Estimation uncertainty for the exogenous variable WSD results from the precipitation measurement errors and the estimation errors of ET_O . Given the various nonlinearities in converting weather variables to ET_O and WSD, a Monte Carlo method is applied to create ensembles for the WSD, where precipitation and ET_O are perturbed with known error parameters.

Precipitation, ET_O and irrigation flow ensembles were post-processed using the Schaake Shuffle method [Clark et al., 2004] and historical records. During the calibration, we used a moving window of 100 days (equivalent to the number for ensembles); either centred, forward shifted or back shifted, depending on the day of the year. These three types of moving window were necessary to given that the irrigation distribution operation is inactive for 3 months (15 May to 15 August) of each year, meaning there is no irrigation flow data for that period. Similar moving windows were used to post-process the irrigation flow ensembles for the evaluation period, but the immediate past year's data were used because observations are unknown ahead of time in an operational forecasting context.

3.2.2.1. Precipitation

Lognormal multiplicative error models have been widely used to generate ensembles for precipitation and to simulate precipitation error in hydrologic data assimilation [Alvarez-Garreton et al., 2014; Li et al., 2014]. Therefore, we used a lognormal multiplicative error to create the ensembles representing measured precipitation:

$$P_{ens} = \zeta_p \times P_{obs} \quad (7)$$

$$\zeta_p \sim LN(\mu_p, \sigma_p) \quad (8)$$

where, P_{ens} is the daily precipitation ensemble member, P_{obs} is observed daily precipitation, ζ_p is the multiplicative error, which follows a lognormal distribution with the mean of μ_p and standard deviation of σ_p .

To create an unbiased precipitation ensemble, μ_p is set to 1 σ_p set to be 0.25 (25% error). This error represents both gauge errors and spatial variability. The assumption of the variance of the precipitation multiplier being 25% is agreed with various studies that have been investigated rain gauge representativeness errors [Barancourt et al., 1992; Ciach and Krajewski, 1999; Villarini et al., 2008] and also consistent with other recent studies [Alvarez-Garreton et al., 2014; DeChant and Moradkhani, 2012; Li et al., 2014]. The representativeness error of rain gauges for areas of order 250 km² is quite variable but of this order. Perera et al. [2015a] found the performance of the ARMAX model was insensitive to choice of individual or

combinations of rain gauges in the area, indicating that the modelling is likely to have relative low sensitivity to this choice.

In accordance with the definition of the lognormal probability distribution model, the natural logarithm of ζ_p , denoted as ζ_p^{LN} , follows a normal distribution with mean and variance given by:

$$\mu = \ln(\mu_p) - \frac{1}{2} \ln \left(1 + \frac{\sigma_p^2}{\mu_p^2} \right) \quad (9)$$

$$\sigma = \sqrt{\ln \left(1 + \frac{\sigma_p^2}{\mu_p^2} \right)} \quad (10)$$

3.2.2.2. Reference Evapotranspiration- ET_O

ET_O was calculated based on the guidelines provided by the United Nations Food and Agricultural Organization Irrigation and Drainage Paper No. 56 (FAO 56) [Allen *et al.*, 1998]. The daily ET_O ensembles were created by perturbing observed weather variables (daily mean air temperature; daily mean dew-point temperature, daily mean wind speed and incoming shortwave solar radiation) using zero mean additive noise. The equations used to calculate the inputs to ET_O are given in Table 4, along with the corresponding measurement accuracy [BoM, 2005] and the standard deviations used in the perturbations. Measurement accuracies were assumed to represent a 3 standard deviation spread [BoM, 2005] and measurement errors were assumed to be independent when calculating the perturbation standard deviations. The perturbation standard deviations account for the number of measurements contributing to each ET_O input.

3.2.3. Forecast Weather Variables

To forecast irrigation demand, forecast weather is required, which has errors resulting from the NWP weather forecasts. NWP models like ACCESS usually contain both systematic biases due to the NWP model structure, site elevation, temporal and spatial resolution and interpolation techniques, together with noise [Perera *et al.*, 2014; Shrestha *et al.*, 2013b]. In constructing irrigation demand ensembles, the NWP weather forecasts should be corrected for bias and the noise should also be represented. The error characteristics of the forecast precipitation are quite different to the forecast errors for ET_O and hence they are treated differently here.

Forecast precipitation ensembles were developed using the approach of Wang *et al.* [2009], which was developed for ACCESS NWP forecasts. This approach uses a simplified version of the Bayesian joint probability technique to derive forecast probability distributions for individual sites as well as for each lead time [Wang *et al.*, 2009]. A joint probability distribution of observations and forecasts is fitted based on past forecast data. Ensemble forecasts are then generated from conditional probability distributions based on the joint probability distribution conditioned on the NWP forecast for that particular day. Space-time correlations are imposed by linking the samples from the forecast probability distributions using the Schaake shuffle [Clark *et al.*, 2004]. Further detail of the post-processing can be found in Robertson *et al.* [2013b].

While the Wang *et al.* [2009] method could potentially also be applied to ET_O forecasts, differences in the distribution characteristics meant this was unsuccessful. An alternative approach based on the analysis of Perera *et al.* [2014] where ACCESS-G NWP weather forecasts were used to generate deterministic daily ET_O forecasts for lead times of 1–9 days. In essence the weather variables input to ET_O were first bias corrected using a regression between forecast and observed data following Perera *et al.* [2014] and then used to

Table 4. Perturbation Methods for ET_O Related Weather Variables^a

Input Estimator	Measurement Accuracy ($\pm 3\sigma$)	Perturbation Standard Deviation
$T_{mean\ ens} = \frac{T_{max} + T_{min} + \zeta_{Temp}}{2}$	0.3 °C	$\sqrt{2} * \frac{0.3}{3}$
$DewPt_{mean\ ens} = \frac{1}{24} \sum_{hr=1}^{24} Dewpt_{hr} + \zeta_{Dewpt}$	0.3 °C	$\sqrt{24} * \frac{0.3}{3}$
$Wndspd_{mean\ ens} = \frac{1}{24} \sum_{hr=1}^{24} Wndspd_{hr} + \zeta_{Wndspd}$	1.03 ms ⁻¹	$\sqrt{24} * \frac{1.03}{3}$
$Srad_{ens} = Srad + \zeta_{Srad}$	1.5 MJ m ⁻²	$\frac{1.5}{3}$

^aDaily mean temperatures ensembles– $T_{mean\ ens}$, daily mean dew point temperatures ensembles– $DewPt_{mean\ ens}$, daily mean wind speed ensembles– $Wndspd_{mean\ ens}$ and daily solar radiation ensembles– $Srad_{ens}$.

make a deterministic ET_O forecast. The errors in that deterministic forecast were then examined against observed ET_O for the relevant climate station. This showed that the ET_O forecast error is multiplicative. Finally, bias-free ensemble daily ET_O forecasts were generated using the deterministic daily ET_O forecasts and forecast error realizations based on the observed multiplicative error and then daily ET_O ensemble forecasts were post-processed using the Schaake Shuffle method as described above.

3.3. Evaluation Methods

The reliability of the ensemble in terms of bias and spread is the most important attribute of ensemble forecasts as it describes the capability of the ensemble spread to represent the real probabilistic uncertainty of the forecast. In this paper, the reliability of ensemble irrigation demand forecasts is quantified using the temporal mean of the ensemble root mean squared error (MRMSE), the mean continuous ranked probability score (CRPS) and one of its decomposition the mean CRPS reliability [Hersbach, 2000], which are defined in equations (11–13) respectively. The MRMSE is derived by calculating the RMSE at each time step using all ensemble members and then averaging the RMSEs for the entire period of interest [Li et al., 2013, 2015]. The mean CRPS and mean CRPS reliability are calculated following step provided by Brown et al. [2010]. The negative orientation of these skill scores leads to 0 for a perfect spread and higher skill scores indicates that forecasts become more biased or the spread less reliable (or both).

The rank histogram approach [Hamill, 2001] is also used to evaluate the reliability of ensemble irrigation demand forecasts. Rank histograms are generated by repeatedly finding the rank of the observation relative to values from the forecast ensemble sorted from lowest to highest. The resulting ranks are then plotted into a histogram. If the ensemble is reliable, the observations should be evenly spread across the various ensemble member ranks. Therefore, a flat rank histogram indicates a reliable ensemble spread; a U-shaped (n-shaped) histogram indicates the ensemble spread is too narrow (wide); and an asymmetric histogram is a sign of bias. Other attributes such as accuracy, sharpness and skill are also important to determine the overall quality of forecasts. Therefore, we further quantify the predictive performance of the mean ensemble daily irrigation demand forecasts through three additional statistical indices, (1) the root mean squared error (RMSE) of the ensemble mean, (2) the Nash-Sutcliffe efficiency coefficient (NS) of the ensemble mean and (3) the mean error (BIAS), which are described in equations (14–16) respectively. We also looked at the ratio between MRMSE and RMSE. This ratio becomes one for a perfect spread, but values less than or more than one indicate ensemble forecasts spreads are under or overestimated, respectively.

All forecast verification scores are normalized using the size of the respective command area to make the predictive performance indicators are independent from the size of the command area (NSE is unaffected by this normalization). The uncertainties of all of the forecast verification scores are evaluated using the bootstrapping technique [Efron and Tibshirani, 1986] and the 5th and 95th confidence intervals are provided along with score.

a. The temporal mean of the ensemble root mean squared error, MRMSE is:

$$\text{MRMSE} = \frac{1}{T} \sum_{t=1}^T \sqrt{\frac{1}{N} \sum_{i=1}^N \left(ID_{fcst,t}^i - ID_{obsv,t} \right)^2} / CA_j \quad (11)$$

b. The mean continuous ranked probability score (CRPS)

$$\text{Mean CRPS} = \frac{1}{T} \sum_{t=1}^T \int_{-\infty}^{\infty} \left(F_{fcst,t}(ID) - F_{obsv,t}(ID) \right)^2 d ID / CA_j \quad (12)$$

$$F_{obsv,t}(ID) = \begin{cases} 0 & (ID < ID_{obsv,t}) \\ 1 & (ID \geq ID_{obsv,t}) \end{cases} \quad (13)$$

c. The root mean squared error, RMSE is:

$$\text{RMSE} = \sqrt{\frac{1}{T} \sum_{t=1}^T \left(\overline{ID}_{fcst,t} - ID_{obsv,t} \right)^2} / CA_j \quad (14)$$

d. Nash–Sutcliffe (NS) model efficiency coefficient (NSE) is:

$$NSE = 1 - \frac{\sum_{i=1}^T (\overline{ID_{fcst,t}^j} - ID_{obsv,t})^2}{\sum_{i=1}^T (\overline{ID_{obsv,t}} - ID_{obsv,t})^2} \quad (15)$$

e. The mean error (BIAS) is:

$$BIAS = \frac{1}{T} \sum_{i=1}^T (\overline{ID_{fcst,t}^j} - ID_{obsv,t}) / CA_j \quad (16)$$

In equations (11–16), $ID_{fcst,t}^j$ is the j^{th} ensemble prediction at time, t , and $ID_{obsv,t}$ is the observed values at t , N is the number of ensembles, T is the total number of time steps $\overline{ID_{fcst,t}^j}$ is the predicted ensemble mean at t , $\overline{ID_{obsv,t}}$ is the mean of $ID_{obsv,t}$ for the period of verification (POV) and CA_j is the size of j^{th} command area.

4. Results

4.1. Precipitation and ET_O Forecast Uncertainties

The exogenous variable, WSD , acts as a weather forcing variable for irrigation demand and it is calculated using precipitation and reference evapotranspiration (ET_O). The forecast and observed uncertainties in these two weather variables contribute to irrigation demand forecast uncertainties. The observation uncertainties for the weather variables are instrument and measurement network dependent, while the forecast uncertainties depend on the forecast skill of the NWP system. The observation uncertainties for weather variables were obtained from the Australian Bureau of Meteorology [BoM, 2005]. For the weather forecasts, ensemble forecasts were first constructed as outlined in section 3.2.3. Detailed evaluations of these ensemble forecasts for the study region were then undertaken through comparisons with local observations. This section briefly evaluates the forecast performance of the precipitation and ET_O ensemble forecasts derived from ACCESS-G.

Table 5 summarizes the statistical indicators related to the forecast performance for precipitation and ET_O ensemble forecasts and Figures 3 and 4 summarize the results for precipitation and evapotranspiration, respectively. These stats are for the periods of 15 August 2010 to 15 May 2011 and 15 August 2011 to 15 May 2012 (551 days). The forecast performance for ensemble daily ET_O and precipitation forecasts declines

Table 5. Statistical Indicators Related to Prediction Performance for Ensemble Precipitation and ET_O Forecasts for Study Area Between 15 August 2010 and 15 May 2011 and 15 May 2012 to 15 May 2012 (551 days)^a

Lead time	Ensemble verification score	Variable	
		Precipitation	ET_O
1 Day	MRMSE mm d ^{−1}	1.89 (1.6–2.19)	1.00 (0.96–1.04)
	Mean CRPS mm d ^{−1}	1.01 (0.79–1.27)	0.37 (0.34–0.39)
	Mean CRPS Rel. mm d ^{−1}	0.06 (0.03–0.12)	0.02 (0.01–0.02)
	RMSE (mean) mm d ^{−1}	4.52 (3.48–5.53)	0.72 (0.67–0.78)
	NSE (mean)	0.51 (0.42–0.62)	0.90 (0.88–0.91)
	BIAS (mean) mm d ^{−1}	−0.69 (−0.98 to −0.43)	−0.09 (−0.13 to −0.04)
3 Day	MRMSE mm d ^{−1}	2.46 (2.12–2.84)	1.37 (1.32–1.43)
	Mean CRPS mm d ^{−1}	1.26 (0.99–1.58)	0.48 (0.45–0.51)
	Mean CRPS Rel. mm d ^{−1}	0.05 (0.03–0.1)	0.03 (0.03–0.04)
	RMSE (mean) mm d ^{−1}	5.67 (4.18–7.11)	0.9 (0.82–0.97)
	NSE (mean)	0.23 (−0.07 to 0.46)	0.84 (0.81–0.87)
	BIAS (mean) mm d ^{−1}	−0.63 (−0.99 to −0.31)	−0.09 (−0.15 to 0.04)
5 Day	MRMSE mm d ^{−1}	2.7 (2.34–3.07)	1.67 (1.61–1.74)
	Mean CRPS mm d ^{−1}	1.34 (1.05–1.64)	0.58 (0.55–0.62)
	Mean CRPS Rel. mm d ^{−1}	0.06 (0.03–0.12)	0.05 (0.04–0.06)
	RMSE (mean) mm d ^{−1}	5.75 (4.42–7)	1.07 (0.99–1.16)
	NSE (mean)	0.2 (0.04–0.37)	0.77 (0.73–0.81)
	BIAS (mean) mm d ^{−1}	−0.66 (−1.02 to −0.34)	−0.14 (−0.21 to −0.08)

^aThe range shown in brackets is the 5th–95th confidence interval from the bootstrapping analysis.

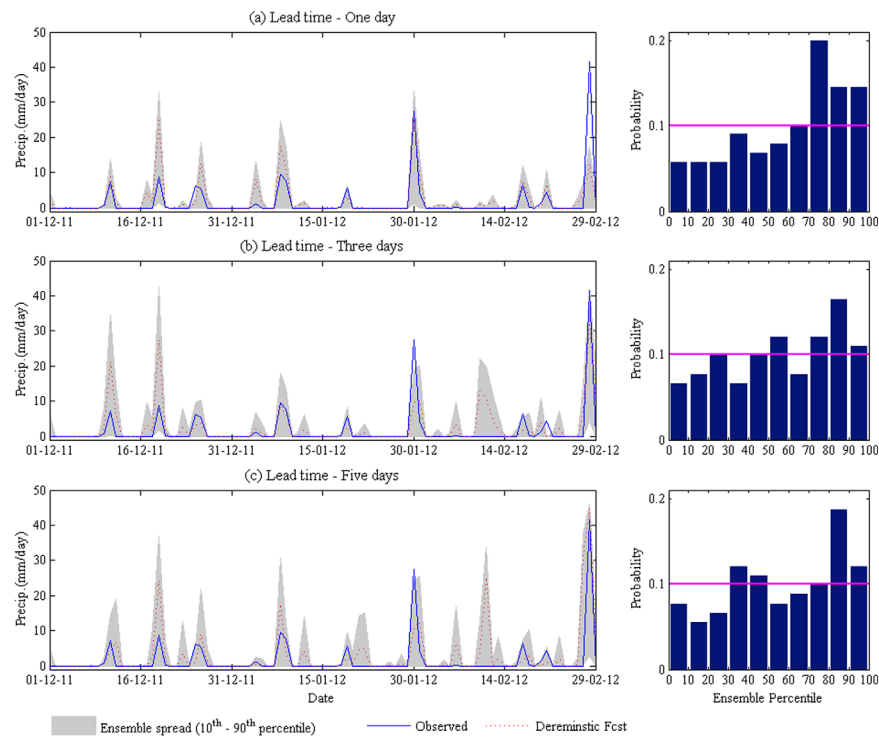


Figure 3. Time series plot (91 days) of observed daily precipitation versus post-process ensemble precipitation forecast and respective rank histograms (551 days) for lead times of 1, 3 and 5 days.

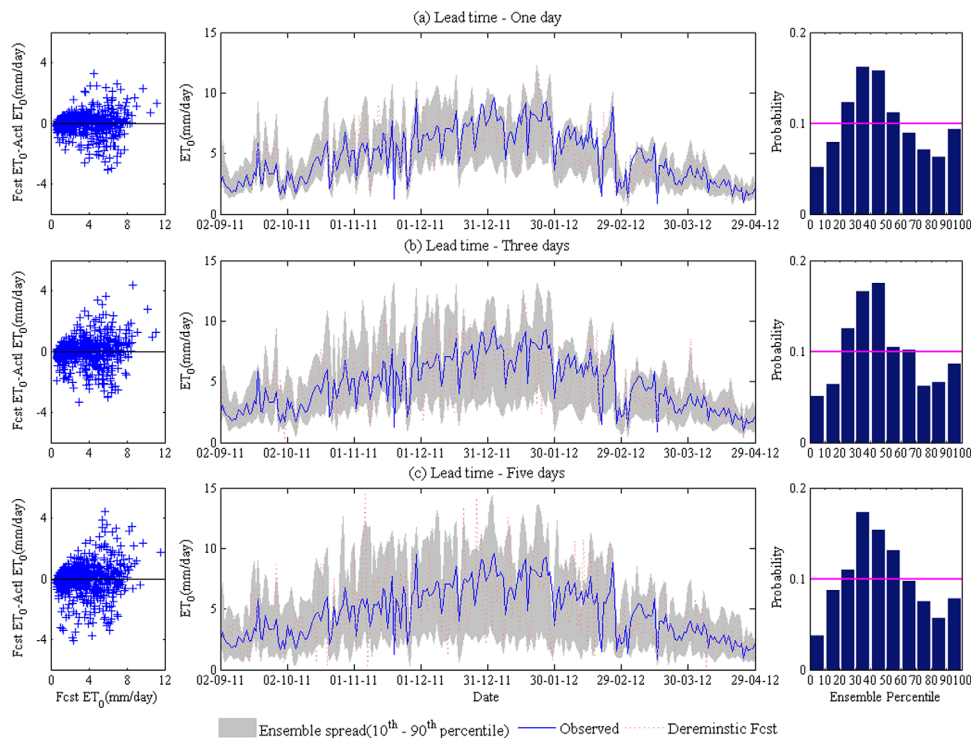


Figure 4. The scatter plot (551 days) between the deterministic daily ET_O forecast and forecast error, time series plot (241 days) of observed daily ET_O versus ensemble daily ET_O forecast with spread between 10th and 90th percentile and respective rank histograms (551 days) for lead times of 1, 3 and 5 days.

Table 6. Average Forecast Performance for Ensemble Daily $ID_{CG\ i, ASP}$ Forecasts Related to the Two Cross Validation Scenarios for Four Channels and Study Area During the Last Year of Calibration Periods 15 August 2010 to 15 May 2011 (274 days) or 15 August 2011 to 15 May 2012 (275 days)^a

Lead Time	Ensemble Verification Score	Average Performances for Command Area				
		CG1	CG2	CG3	CG4	CG1234
1 Day	MRMSE	0.39	0.41	0.32	0.36	0.25
	(ML d ⁻¹ km ⁻¹)	(0.38–0.41)	(0.39–0.42)	(0.31–0.33)	(0.34–0.37)	(0.24–0.26)
	Mean CRPS	0.21	0.19	0.12	0.11	0.08
	(ML d ⁻¹ km ⁻¹)	(0.2–0.22)	(0.18–0.2)	(0.11–0.12)	(0.1–0.11)	(0.08–0.08)
	Mean CRPS Rel	0.05	0.01	0.01	0.03	0.01
	(ML d ⁻¹ km ⁻¹)	(0.04–0.06)	(0.01–0.02)	(0.01–0.01)	(0.02–0.03)	(0.01–0.01)
	RMSE (mean)	0.38	0.34	0.2	0.15	0.12
	(ML d ⁻¹ km ⁻¹)	(0.36–0.41)	(0.32–0.36)	(0.19–0.22)	(0.14–0.16)	(0.12–0.13)
	NSE (mean)	0.46	0.73	0.83	0.91	0.94
	(ML d ⁻¹ km ⁻¹)	(0.37–0.52)	(0.69–0.75)	(0.8–0.85)	(0.9–0.92)	(0.93–0.94)
3 Day	BIAS (mean)	0.1	0.06	0.04	0.05	0.03
	(ML d ⁻¹ km ⁻¹)	(0.08–0.13)	(0.03–0.08)	(0.03–0.06)	(0.04–0.06)	(0.02–0.04)
	MRMSE	0.48	0.49	0.37	0.38	0.32
	(ML d ⁻¹ km ⁻¹)	(0.46–0.5)	(0.47–0.51)	(0.36–0.38)	(0.36–0.39)	(0.31–0.33)
	Mean CRPS	0.27	0.25	0.17	0.14	0.13
	(ML d ⁻¹ km ⁻¹)	(0.25–0.29)	(0.24–0.26)	(0.16–0.18)	(0.14–0.15)	(0.13–0.14)
	Mean CRPS Rel.	0.06	0.02	0.01	0.01	0
	(ML d ⁻¹ km ⁻¹)	(0.06–0.08)	(0.02–0.03)	(0.01–0.01)	(0.01–0.01)	(0–0.01)
	RMSE (mean)	0.48	0.44	0.3	0.25	0.24
	(ML d ⁻¹ km ⁻¹)	(0.45–0.51)	(0.42–0.46)	(0.28–0.31)	(0.23–0.26)	(0.22–0.25)
5 Day	NSE (mean)	0.17	0.55	0.64	0.76	0.77
	(ML d ⁻¹ km ⁻¹)	(0.07–0.22)	(0.51–0.59)	(0.6–0.67)	(0.73–0.78)	(0.74–0.8)
	BIAS (mean)	0.1	0.04	0.03	0.05	0.04
	(ML d ⁻¹ km ⁻¹)	(0.06–0.13)	(0.01–0.07)	(0.01–0.05)	(0.03–0.07)	(0.02–0.06)
	MRMSE	0.48	0.52	0.39	0.37	0.35
	(ML d ⁻¹ km ⁻¹)	(0.46–0.5)	(0.5–0.53)	(0.38–0.4)	(0.36–0.38)	(0.34–0.36)
	Mean CRPS	0.27	0.27	0.19	0.15	0.16
	(ML d ⁻¹ km ⁻¹)	(0.25–0.29)	(0.26–0.29)	(0.18–0.2)	(0.15–0.16)	(0.15–0.17)
	Mean CRPS Rel.	0.07	0.02	0.01	0	0.01
	(ML d ⁻¹ km ⁻¹)	(0.06–0.08)	(0.02–0.03)	(0.01–0.02)	(0–0.01)	(0–0.01)

^aThe range shown in brackets is the 5th - 95th confidence interval from the bootstrapping analysis.

with increasing lead time, as expected. For precipitation forecasts, the MRMSE, mean CRPS and RMSE increase approximately 42%, 32% and 27% respectively and mean CRPS reliability remain same, as the lead time increases from 1 to 5 days. For ET_O forecasts the MRMSE, mean CRPS, mean CRPS reliability and RMSE increase more than twice for lead time 5 days and indicated spread of ET_O ensemble forecasts is poor reliable for longer lead times. The NS efficiency coefficient for mean precipitation and ET_O ranged between 0.51 and 0.20 and between 0.90 and 0.77, respectively, for lead times of 1–5 days. The rank histogram and bias shows that the ensemble precipitation forecast was slightly negatively biased and that the ensemble ET_O forecast was slightly positively biased and the uncertainty was overestimated for ET_O . The results also suggest that the forecast performance for ET_O was higher than for precipitation.

4.2. Ensemble Demand Forecasts for the Model Calibration Period

The model parameters reported in Perera *et al.* [2015a] are used here. The following results are based on forecasts for the 2010–2011 and 2011–2012 irrigation seasons. The deterministic model was calibrated to the 2006–2007, 2007–2008, 2008–2009 and 2009–2010 seasons plus one of 2010–2011 or 2011–2012. Independent validation results were obtained for each of the 2010–2011 and 2011–2012 irrigation seasons. Tabulated values below were obtained by calculating the calibration (or validation) metrics for each of the two seasons and then averaging these. We note that the “calibration period” results correspond to only 1 of the 5 years contributing to the original model fitting.

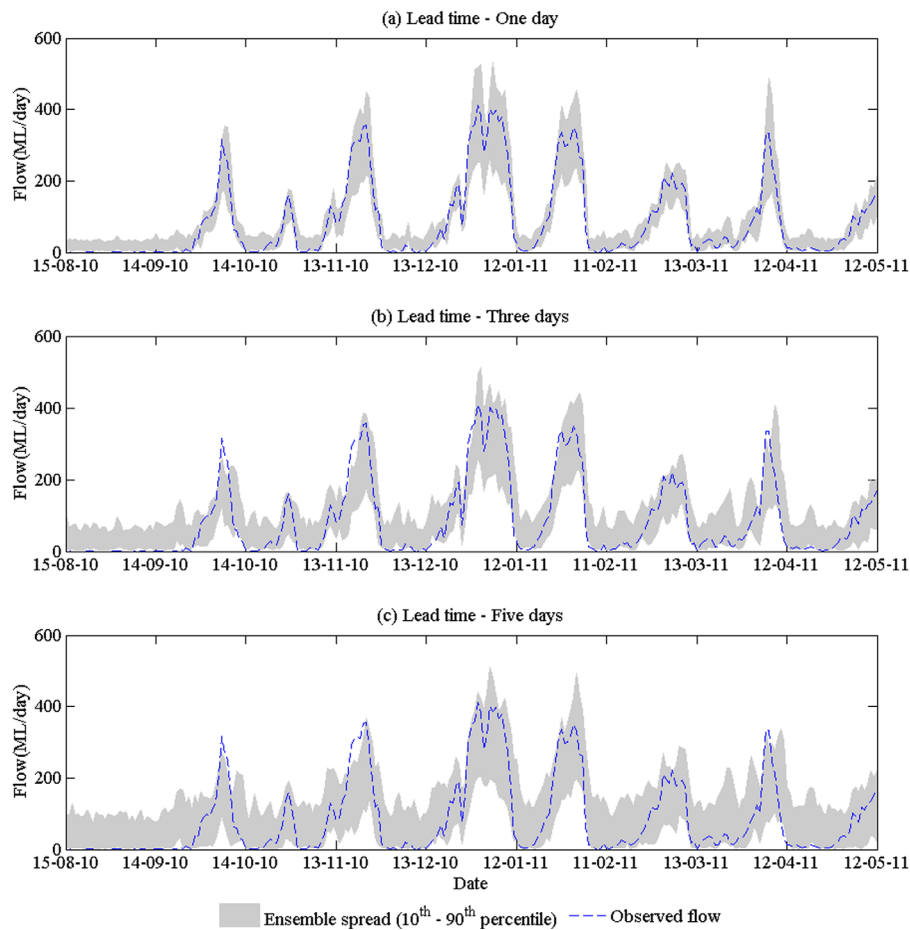


Figure 5. Time series plot of observed versus ensemble daily $ID_{CG\ 1234, ASP}$ forecasts with the ensemble spread between 10th and 90th percentile for lead times of 1, 3 and 5 days for irrigation year 15 August 2010 to 15 May 2011 (274 days-validation scenario 1 in the Table 5).

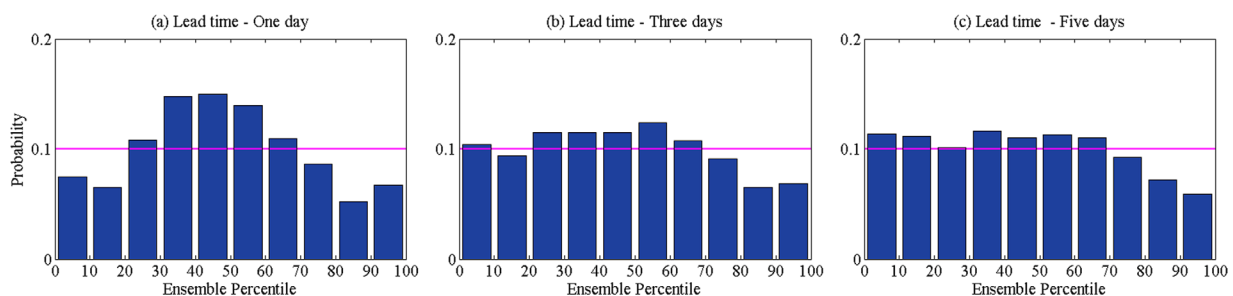


Figure 6. Rank histograms for observed and ensemble daily $ID_{CG\ 1234, ASP}$ forecasts for lead times of 1, 3, and 5 for irrigation years 15 August 2010 to 15 May 11 (274 days-validation scenario 1 in the Table 5).

Table 6 provides the average statistical indicators between two calibration scenario for ensemble daily $ID_{CG\ i, ASP}$ forecasts across all 5 command areas and the performance for each individual calibration scenario is in supporting information Table S1. These calibration periods have 4 years in common, with the fifth year being different between the two sets of results and the results in Table 6 only represent the average of those fifth year. Only the results relating to the best LOOCV calibration scenario and the full study area (i.e., LOOCV-S 1 for CG 1234) are shown graphically as time series (Figure 5) and rank histograms (Figure 6). The statistical indicators for the two scenarios corresponding to each command area vary significantly due to the differences in irrigation flows between years. We start by considering

Table 7. Average Forecast Performance for Ensemble Daily $ID_{CG\ i, ASP}$ Forecasts Related to the Two Cross-validation Scenarios for Four Channels and Study Area During the Evaluation Periods 15 August 2010 to 15 May 2011 (274 days) or 15 August 2011 to 15 May 2012 (275 days)^a

Lead Time	Ensemble Verification Score	Average Performances for Command Area				
		CG1	CG2	CG3	CG4	CG1234
1 Day	MRMSE	0.35	0.39	0.31	0.35	0.23
	(ML d ⁻¹ km ⁻¹)	(0.34–0.36)	(0.38–0.4)	(0.3–0.33)	(0.33–0.37)	(0.22–0.25)
	Mean CRPS	0.17	0.15	0.1	0.1	0.07
	(ML d ⁻¹ km ⁻¹)	(0.16–0.17)	(0.14–0.16)	(0.1–0.11)	(0.1–0.11)	(0.07–0.07)
	Mean CRPS Rel.	0.03	0.02	0.02	0.04	0.02
	(ML d ⁻¹ km ⁻¹)	(0.03–0.04)	(0.01–0.02)	(0.02–0.02)	(0.03–0.04)	(0.02–0.02)
	RMSE (mean)	0.3	0.27	0.15	0.11	0.09
	(ML d ⁻¹ km ⁻¹)	(0.28–0.31)	(0.26–0.28)	(0.14–0.16)	(0.1–0.11)	(0.08–0.09)
	NSE (mean)	0.63	0.82	0.9	0.95	0.96
		(0.55–0.68)	(0.79–0.83)	(0.88–0.91)	(0.94–0.96)	(0.96–0.97)
3 Day	BIAS (mean)	0.1	0.01	0.02	0.02	0.01
	(ML d ⁻¹ km ⁻¹)	(0.08–0.11)	(0–0.03)	(0.01–0.03)	(0.02–0.03)	(0–0.02)
	MRMSE	0.41	0.46	0.35	0.36	0.28
	(ML d ⁻¹ km ⁻¹)	(0.4–0.42)	(0.44–0.47)	(0.34–0.36)	(0.35–0.37)	(0.28–0.29)
	Mean CRPS	0.2	0.21	0.13	0.12	0.11
	(ML d ⁻¹ km ⁻¹)	(0.19–0.21)	(0.2–0.22)	(0.13–0.14)	(0.12–0.13)	(0.1–0.11)
	Mean CRPS Rel.	0.04	0.04	0.02	0.02	0.01
	(ML d ⁻¹ km ⁻¹)	(0.04–0.05)	(0.03–0.05)	(0.01–0.02)	(0.02–0.02)	(0.01–0.02)
	RMSE (mean)	0.37	0.39	0.25	0.2	0.18
	(ML d ⁻¹ km ⁻¹)	(0.35–0.39)	(0.37–0.4)	(0.23–0.26)	(0.19–0.21)	(0.18–0.19)
5 Day	NSE (mean)	0.44	0.64	0.74	0.84	0.86
		(0.32–0.51)	(0.6–0.67)	(0.71–0.77)	(0.82–0.85)	(0.84–0.87)
	BIAS (mean)	0.09	–0.04	–0.02	–0.01	–0.01
	(ML d ⁻¹ km ⁻¹)	(0.07–0.12)	(–0.06 to –0.01)	(–0.03 to 0)	(–0.03 to 0)	(–0.03 to 0)
	MRMSE	0.41	0.48	0.37	0.37	0.31
	(ML d ⁻¹ km ⁻¹)	(0.4–0.43)	(0.46–0.5)	(0.35–0.38)	(0.36–0.39)	(0.3–0.32)
	Mean CRPS	0.21	0.23	0.15	0.14	0.13
	(ML d ⁻¹ km ⁻¹)	(0.2–0.22)	(0.22–0.24)	(0.15–0.16)	(0.14–0.15)	(0.13–0.14)
	Mean CRPS Rel.	0.05	0.05	0.03	0.03	0.02
	(ML d ⁻¹ km ⁻¹)	(0.04–0.06)	(0.04–0.06)	(0.02–0.03)	(0.02–0.03)	(0.02–0.03)
	RMSE (mean)	0.38	0.43	0.29	0.25	0.24
	(ML d ⁻¹ km ⁻¹)	(0.36–0.4)	(0.41–0.45)	(0.28–0.3)	(0.24–0.26)	(0.23–0.25)
	NSE (mean)	0.42	0.57	0.65	0.75	0.76
		(0.31–0.49)	(0.52–0.6)	(0.61–0.68)	(0.73–0.77)	(0.74–0.79)
	BIAS (mean)	0.09	–0.07	–0.04	–0.05	–0.04
	(ML d ⁻¹ km ⁻¹)	(0.06–0.11)	(–0.09 to –0.04)	(–0.06 to 0.02)	(–0.07 to 0.04)	(–0.05 to 0.02)

^aThe range shown in brackets is the 5th - 95th confidence interval from the bootstrapping analysis.

the ensemble mean forecast. The NSE between forecast and observed irrigation demand ranged between 0.91 (1 day lead time, CG 1234) and 0.31 (5 day lead time, CG 1). The highest and lowest NSE values were always found at CG 1234 and CG 1, respectively due to differences in the area irrigated and number of supply points. For 5 day lead times compared with 1 day lead times, NSE decreased by more than 40% for small command areas (CG 1, CG 2 and CG 3) and approximately 25% for larger command areas (CG 4 and CG 1234). The bias was highest at CG 1234 and lowest at CG 1 and it is proportional to the size of the area irrigated. The bias showed that the ensemble daily demand forecasts slightly over predicted the observed flows for all command areas and mostly remains approximately same with increased in lead time. .

The ensemble spread can be evaluated through the MRMSE, mean CRPS, mean CRPS reliability, RMSE and the rank histograms. The difference between MRMSE and RMSE increased with the increasing command area or decreasing lead times. The mean CRPS, mean CRPS reliability and difference between these two scores increased with the increasing command area or lead times. These facts suggest that reliability of ensemble spread declines with increasing command area or lead times. The MRMSE was higher than the corresponding RMSE for all command areas and for all lead times. Across the five command areas, MRMSE, mean CRPS, mean CRPS reliability and RMSE increase on average by approximately 23%, 53%, 8% and 73% respectively from 1 day to 5 days lead time. For most cases, these statistics and the rank histograms (Figure 6) show that the ensemble spread marginally overestimated the forecast error variability for the first day and then tend to be flat with increased in lead time, indicating a reliable ensemble spread. During the

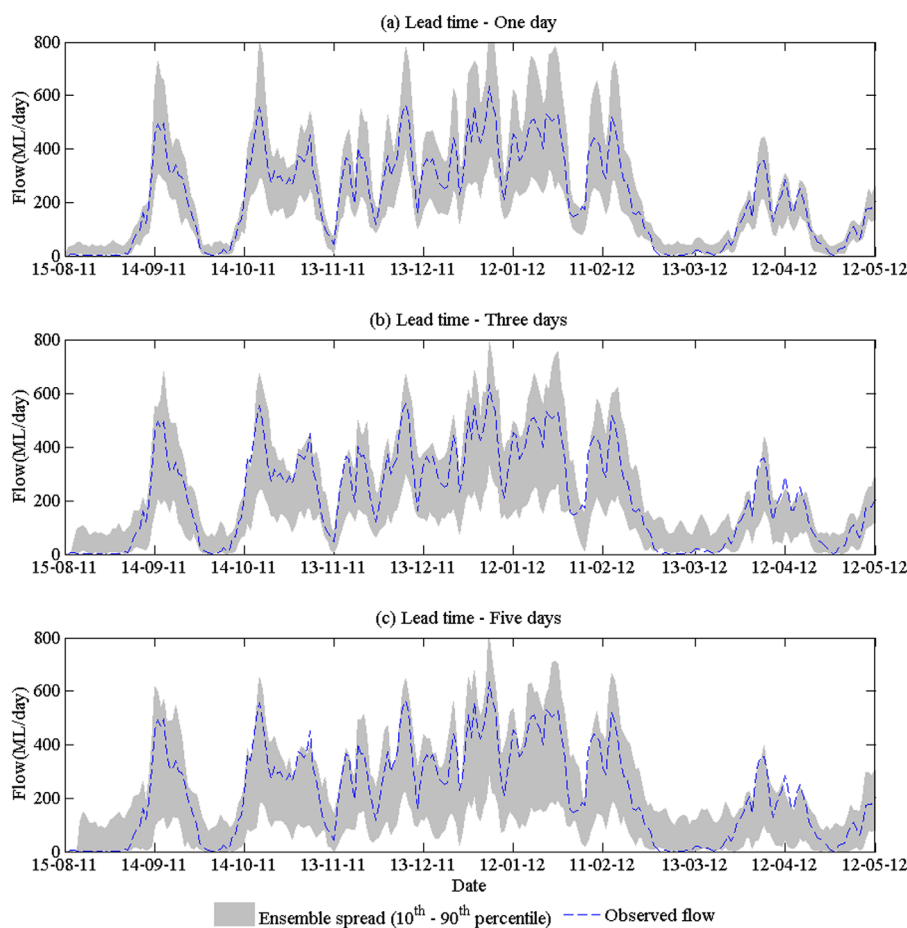


Figure 7. Time series plot of observed versus ensemble daily $ID_{CG\ 1234, ASP}$ forecasts with the ensemble spread between 10th and 90th percentile for lead times of 1, 3 and 5 for irrigation year 15 August 2011 to 15 May 2012 (275 days).

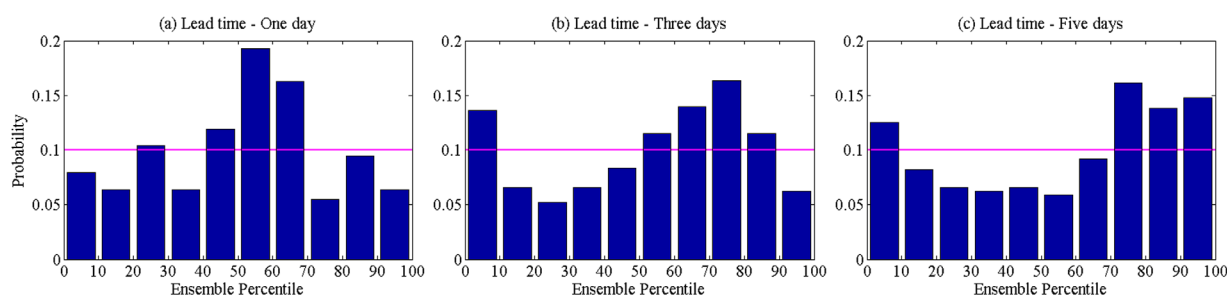


Figure 8. Rank histograms for observed and ensemble daily $ID_{CG\ 1234, ASP}$ forecasts for lead times of 1, 3, and 5 days during irrigation year 15 August 2011 to 15 May 2012 (275 days).

calibration periods, the observed daily $ID_{CG\ 1234, ASP}$ values were within the ensemble daily $ID_{CG\ i, ASP}$ forecast spread (10th–90th percentile) for 86%, 83% and 82% of the time with respect to lead time 1, 3 and 5 days.

4.3. Real-Time Forecasting With Numerical Weather Prediction Outputs

We now examine the results for validation conditions using a similar approach to the previous section. With the exception of the fitting of uncertainty parameters for the NWP ensembles, these demand forecasts are made under operational conditions; that is using observation data available from automatic weather stations, the SCADA network of supply points and NWP forecast data, all of which would be available at the time of making an operational forecast, and with the ARMAX model fitted to independent data. The aim is

to test the forecast performance of both the ensemble mean and to assess how well the ensemble represents the forecast uncertainty.

Table 7 provides the average statistical indicators between two evaluation scenario for ensemble daily $ID_{CG\ i, ASP}$ forecasts across all 5 command areas and the performance for each individual evaluation scenario is in supporting information Table S2. Figure 7 shows the time series plots of observed and ensemble daily demand forecast for evaluation year 2011/2012, while Figure 8 shows the rank histograms and associated probabilities. The NSE values ranged between 0.97 (1 day lead time, CG 4) and 0.22 (5 day lead time, CG 1) and for the whole study area it ranged between 0.97 and 0.75 for 1 and 5 day lead times, respectively. The bias varied with the evaluation year, being positive for 2010/2011 and negative for 2011/2012. This is partly reflects the variability of irrigation flow within each year, where the highest variability occurred during year 2011/2012.

The ensemble spread is again examined by using MRMSE, mean CRPS, mean CRPS reliability, RMSE and rank histograms. In general all MRMSE, mean CRPS, mean CRPS reliability and RMSE decrease with increasing irrigated area reflecting the higher forecast performances for larger command areas and the spread of forecast uncertainties is not reliable for smaller command areas. The pattern between the MRMSE, mean CRPS, mean CRPS reliability and RMSE was similar to calibration period, where MRMSE is higher for all command areas and all lead times. The difference between MRMSE and RMSE increased and the difference between mean CRPS and mean CRPS reliability decreased with the increasing command area and decreasing lead times. Typically MRMSE is larger than RMSE values indicating that the ensemble spread is somewhat overestimating the forecast uncertainty at system scale, when irrigation flow among distribution channels aggregated. The average ratio MRMSE/RMSE across 2 validation years varies between 1.10 and 4.20 for all command areas for 1 day lead time. Ideally this ratio should be one and significant deviations from one indicate that the ensemble spread is unreliable. For the small command areas (CG 1 and CG 2) MRMSE/RMSE varies between 1.16 and 1.44, indicating the ensemble spread is slightly overestimated for the smaller command areas and consistently overestimated for the larger command areas. The rank histograms for the whole study area show that the ensemble is marginally too wide and slightly negative biased for 1 day lead time. This negative bias increases with lead time and forecast ensemble spreads are slightly under-dispersive for lead times of 3 and 5 days. This is consistent with the indications from mean CRPS, mean CRPS reliability and MRMSE versus RMSE; however, those statistics are likely to be more sensitive to outliers than the rank histograms. During the evaluation periods, the observed daily $ID_{CG\ 1234, ASP}$ values were within the ensemble daily $ID_{CG\ i, ASP}$ forecasts spread (10th–90th percentile) for 86%, 80% and 72% times for lead times of 1, 3 and 5 days respectively. Overall, these results suggest that the ensemble forecasts give good estimates of forecast uncertainty and reliable probabilistic irrigation demand forecasts, particularly for the large command areas, but that the ensemble spread does not grow quickly enough with time.

5. Discussion

The ensemble forecasting techniques used here build on those used in forecasting short runoff or stream flow [Addor et al., 2011; Bennett et al., 2014; Robertson et al., 2013a; Shrestha et al., 2013a; Smiatek et al., 2012]. Those studies have either used stochastic precipitation forecasts that have been post-processed or output from NWP models. While, the inputs and the techniques are similar for forecasting stream flows and irrigation demands, the dynamic responses of the systems are the opposite; with irrigation demand decreasing when precipitation increases and evapotranspiration decreases and streamflow doing the opposite. In catchments there is also likely to be more variation in antecedent conditions prior to precipitation events (antecedent moisture tends to be controlled by the application of irrigation in irrigated fields). This means that the forecast performance is not directly comparable between streamflow and irrigation demand.

The forecast performance for the ensemble irrigation demand predictions were evaluated for lead times of 1–5 days across the four command areas plus the full study area. Both the average forecasts (ensemble means) and the uncertainty estimates (ensemble spread) performed well overall. NSEs for forecast conditions were up to 0.97 for 1 day lead time and larger command areas and remained above 0.65 for 5 day lead times, with the exception of the two smallest command areas. There were clear dependencies on lead time and command area. The area dependence relates to the amount of averaging between individual irrigation farms while the dependence on lead time relates to accumulation of forecast errors over time.

From the system operators' perspective, these probabilistic short-term system scale irrigation demand forecasts could assist with planning operations, particularly those operations such as transferring water from the main storage at Lake Eildon to the irrigation command areas. The ensemble approach provides a reliable estimate of forecast uncertainty that could be used to inform operational risks. The modelling also provides a quantitative link to enable operational weather forecasts to be more easily utilized in system operation decisions.

From the forecasting context, this is the first study to generate probabilistic daily irrigation demand forecasts with lead times up to 5 days at the system scale. The results showed that the forecasting performance for ensemble daily irrigation demand forecasts were higher than most previous studies [Alfonso *et al.*, 2011; Pulido-Calvo and Gutierrez-Estrada, 2009; Tian and Martinez, 2014; Ticlavilca *et al.*, 2011] and the performance of the forecasted ensemble mean is marginally lower than the deterministic forecasts derived by Perera *et al.* [2015a] using the same time series model. The rank histograms highlighted that the spreads were slightly over dispersive for lead time 1 and then change to slightly under-dispersive as lead time increases. This implies the influence of other sources of uncertainty that are not being fully captured by input errors. There are a number of influences not explicitly included in the model. These include responses to regular (\sim monthly) adjustments in yearly water allocation, changes in the price of water in the market, variations in sowing date for crops, on-farm storages and stock and domestic (non-irrigation) water leading to additional errors. These are in general model structural uncertainties, which we have not dealt with this paper.

There are some subtle differences in the evolution of ensemble spread in different situations. In general, where there is a low antecedent flow, the 1 day lead time spread is small and it increases with antecedent flow. The low initial spread is due primarily to the multiplicative error applied to the observed flows, which has the largest influence on the lead one ARMAX outputs. The evolution of the ensemble spread over time is influenced by both the initial ensemble spread and the contributions to spread from the error component of the ARMAX model and the weather forecasts. The error structure for the observe ET_o is complicated by its propagation from measurements through the Penman-Monteith equation. The inputs to the observed ET_o calculation are assumed to have additive errors. The precipitation observation error model is multiplicative. These choices of measurement error structure reflect the nature of measurement errors for the different

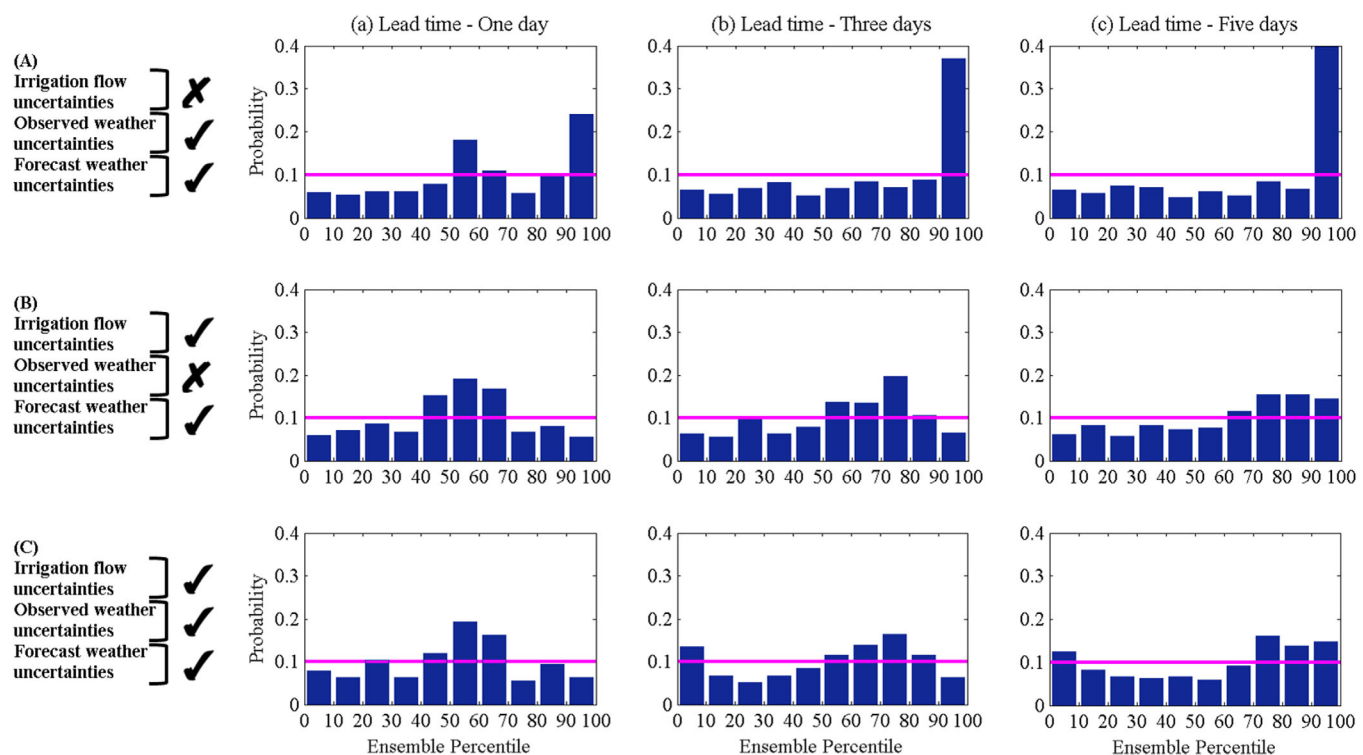


Figure 9. Rank histograms (a) Excluding irrigation flow uncertainties (b) Excluding observed weather uncertainties and (c) Including irrigation flow and observed and forecast weather uncertainties, for observed and ensemble daily $ID_{CG, 1234, ASP}$ forecasts for lead times of 1, 3, and 5 days during the evaluation period 15 August 2011 to 15 May 2012 (275 days).

types of instruments involved. The ensemble evolution is influenced by the error structure in the ARMAX model itself and the weather forecasts. The ARMAX model has an additive error structure, which is justified by the forecast errors from the deterministic ARMAX model [Perera *et al.*, 2015a, Figures 8 and 9]. The forecast ET_O also has an additive error structure, justified by error analysis in Perera *et al.* [2014], Figure 7. The precipitation forecast errors are determined by the structure of the Bayesian Joint Probability model [Robertson *et al.*, 2013a; Wang *et al.*, 2009]. Of these, the additive errors in the ARMAX model have the greatest effect on the ensemble evolution under different conditions and they lead to rapid ensemble widening when the initial spread is small but slow widening when the initial spread is larger.

As discussed in the previous paragraph, there are a variety of sources of uncertainty incorporated into the ensembles, including uncertainty in antecedent conditions (observed flow/demand, observed weather) and forecast weather uncertainty. To further understand the importance of the antecedent conditions in contributing to the ensemble variability, we undertook two additional sets of simulations. The first excluded uncertainty in the antecedent flow and the second excluded uncertainty in the antecedent weather. Figure 9 shows the resulting rank histograms. The top row of histograms indicates that the ensembles become biased when flow uncertainty is excluded. Comparing the middle and lower rows in Figure 9 shows that including the impact of antecedent weather uncertainty also leads to subtle improvements in the ensemble (less under-dispersion, slightly less bias), but the improvements are smaller than the effect of antecedent flow. These results suggest that including the antecedent conditions as a source of uncertainty is important and that flow is more important than past weather. The difference in influence of past flow and past weather is as expected given that the ARMAX model weights past flows more heavily than past weather.

In this paper, the input error terms are assumed to be independently and identically distributed. These assumptions are not valid in practice because the time series plots show a serial correlation of the irrigation demand forecast error. This might be due to structural errors in the model but could also be partly due to serial correlation of the ET_O forecast error as the serial correlation of the precipitation error was corrected using the post-processing approach following Robertson *et al.* [2013b]. This serial correlation of irrigation demand forecast error is highly subjective for non-stationary time series like previous irrigation flows and accordingly, the systematic bias increased with the increase in lead time. However, in the face of higher autocorrelation between consecutive observed irrigation flows, the serial correlation of ET_O forecast error is not significant. Nevertheless, ensemble forecasting scheme has provided sufficiently accurate probabilistic irrigation demand forecasts that can be useful to the system operators for their routine irrigation distribution decisions.

6. Conclusion

This paper developed an ensemble forecasting scheme to generate a real-time probabilistic short-term system scale irrigation demand forecasts. We used a deterministic multivariate time series model that was developed previously [Perera *et al.*, 2015a], along with real-time data recorded at irrigation regulators; short-term weather forecast derived from an NWP model and observed weather variables recorded at automatic weather stations. This method was applied to four neighbouring irrigated agricultural areas operating under fully automated irrigation distribution system.

The observation, estimation and forecast uncertainties were guided by the manufacturer's specification, obtained from the literature or calculated. A range of perturbation methods were used to generate ensemble for each input that is necessary for the deterministic time series models. The spatial and temporal predictive performance for probabilistic daily irrigation demand forecast ($ID_{CG\ i, ASP}$ and $ID_{CG\ i, OTR}$) were evaluated against observed data recorded at 1016 service points. Averaged over the two evaluation periods, the NSE values for $ID_{CG\ i, ASP}$ across the 5 command areas were in the range 0.96 (CG 1234) - 0.63 (CG 1) for 1 day lead time and between 0.76 (CG1234) and 0.42 (CG 1) for 5 days lead time. The predictive performance improved as the irrigation area served by the channel increased and the temporal predictive performances declined with the lead time. The rank histograms showed that the ensemble spread was slightly over dispersive for shorter lead time (1–2 days) and slightly under-dispersive for longer lead time (3–5 days), suggesting that additional sources of error that are not accounted for accumulate over time.

This study investigated input uncertainties in detail and overlooks the model structural and parameter uncertainties. While preliminary trials showed parameter uncertainties have little influence, it would be valuable to examine ways of including model structural uncertainty. Nevertheless, the ensemble forecasting

scheme adopted provides useful information on demand forecast uncertainty that would be useful in helping system operator manage the risk associated with operational decisions.

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